

Datasheet

Safe working pressures have traditionally been expressed as proportions of either the burst pressure or yield point of a tube. These proportions have varied over time as production methods have improved and steels have evolved. Different industries and pressure vessel codes have also adopted different standard practices.

The most common ratio used over the past 50 years has probably been 4:1 burst pressure max. operating pressure. However, some codes are now reducing this factor to 3.5 or even 3. The problem with using this factor for modern austenitic stainless steels is that it does not permit the mechanical properties of such steels to be used to their maximum potential. Therefore for such materials a factor of 1.5 or 1.6 x yield pressure has become customary.

Pressure calculating formulae

For calculating internal pressure (hoop stress) the most common formulae are the simple.

| | |
|-----------------------|---------------------|
| Barlow formula | $P = \frac{2St}{D}$ |
|-----------------------|---------------------|

or the more precise **Lamé formula** which can be calculated using either OD/WT or OD/ID. The two versions are as follows:

| | |
|-------|---|
| OD/WT | $P = \frac{2St(D-t)}{D^2 - 2Dt + 2t^2}$ |
| OD/ID | $P = S(D^2 - d^2)$ |

The Barlow formula is useful for quick ballpark calculations but in general it is best to use the Lamé formula as this will give a more precise answer.

For all the formulae, the symbols have the following meanings:

| | |
|------------|--|
| P | = Internal pressure |
| S | = Proof Stress or UTS for calculating yield or burst pressure respectively |
| t | = Wall thickness |
| D | = Outside diameter |
| d | = Inside diameter |
| WT | = Wall thickness |
| UTS | = Ultimate tensile strength |

The suitable "working or operating" pressure is taken as the pressure at which the tube will permanently yield (Rp 0.2 or Rp 1.0) minus a safety factor. The pressure at which a tube will fail or burst is taken as the pressure required to exceed the tensile strength (Rm) minus a safety factor.

When asked "What pressure is a tube good for?", Fine Tubes can only state the minimum (theoretical) yield and burst pressures of a particular tube at room temperature and state that the end user must decide what the safe maximum working pressure should be based on this information. It should also be noted that these results assume the tubing is subject to no other stresses that would influence the calculations. This is because Fine Tubes can never be sure of the environmental conditions in which the tube will be used or the appropriate safety factor for that application.

Calculating Collapse Pressure

The formula for calculating collapse pressure is
In this case S = UTS only.

| |
|----------------------------|
| $P = \frac{2St(D-t)}{D^2}$ |
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Based on the shown formulae the nominal yield, burst and collapse pressures of common sizes at room temperature have been calculated and are shown below.

| Size | Material | Burst | Distension (0.2% Proof) | Distension (1% Proof) | Collapse |
|------------|-----------|--------|-------------------------|-----------------------|----------|
| ¼" x 0.035 | 316L | 22,200 | 8,700 | 10,400 | 16,900 |
| ¼" x 0.035 | Alloy 400 | 22,200 | 8,900 | 9,400 | 16,900 |
| ¼" x 0.035 | Alloy 825 | 27,000 | 11,100 | 12,200 | 20,500 |
| ¼" x 0.035 | Alloy 625 | 38,100 | 19,100 | 20,500 | 28,900 |
| ¼" x 0.049 | 316L | 32,100 | 12,600 | 14,900 | 22,000 |
| ¼" x 0.049 | Alloy 400 | 32,100 | 12,800 | 13,600 | 22,000 |
| ¼" x 0.049 | Alloy 825 | 39,000 | 16,000 | 17,600 | 26,700 |
| ¼" x 0.049 | Alloy 625 | 55,000 | 27,500 | 29,600 | 37,700 |
| ¼" x 0.065 | 316L | 43,800 | 17,200 | 20,400 | 26,900 |
| ¼" x 0.065 | Alloy 400 | 43,800 | 17,500 | 18,600 | 26,900 |
| ¼" x 0.065 | Alloy 825 | 53,100 | 21,900 | 24,000 | 32,700 |
| ¼" x 0.065 | Alloy 625 | 75,100 | 37,500 | 40,300 | 46,200 |
| ⅜" x 0.035 | 316L | 14,300 | 5,600 | 6,700 | 11,900 |
| ⅜" x 0.035 | Alloy 400 | 14,300 | 5,700 | 6,100 | 11,900 |
| ⅜" x 0.035 | Alloy 825 | 17,300 | 7,100 | 7,800 | 14,400 |
| ⅜" x 0.035 | Alloy 625 | 24,500 | 12,200 | 13,200 | 20,300 |
| ⅜" x 0.049 | 316L | 20,500 | 8,100 | 9,600 | 15,900 |
| ⅜" x 0.049 | Alloy 400 | 20,500 | 8,200 | 8,700 | 15,900 |
| ⅜" x 0.049 | Alloy 825 | 24,900 | 10,300 | 11,200 | 19,300 |
| ⅜" x 0.049 | Alloy 625 | 35,200 | 17,600 | 18,900 | 27,200 |
| ⅜" x 0.065 | 316L | 28,100 | 11,100 | 13,100 | 20,100 |
| ⅜" x 0.065 | Alloy 400 | 28,100 | 11,200 | 11,900 | 20,100 |
| ⅜" x 0.065 | Alloy 825 | 34,100 | 14,100 | 15,400 | 24,400 |
| ⅜" x 0.065 | Alloy 625 | 48,200 | 24,100 | 25,900 | 34,400 |

Appropriate working pressures will depend on the environment, application and design code. These must be decided by the end user on the basis of the mechanical data given above.

Typical mechanical properties are as follows:

| Material | Rp 0.2 | | Rp 1.0 | | Rm | | Elongation 2" GL or 5.65 √ 50 |
|----------|--------|-------|--------|-----|------|-----|----------------------------------|
| | MPa | ksi | MPa | ksi | MPa | ksi | |
| 316L | 190 | 27.55 | 225 | 33 | 485 | 70 | 35% |
| A825 | 241 | 35 | 265 | 38 | 586 | 85 | 30% |
| A400 | 193 | 28 | 205 | 30 | 483 | 70 | 35% |
| A625 | 414 | 60 | 445 | 64 | 827 | 120 | 30% |
| 4429 | 295 | 43 | 330 | 48 | 580 | 84 | 35% |
| S31803 | 450 | 65 | | | 620 | 90 | 25% |
| S32750 | 550 | 80 | | | 800 | 116 | 15% |
| Alloy 33 | 380 | 55 | 420 | 61 | 720 | 104 | 40% |
| Ti325 | 730 | 105 | | | 900 | 130 | 15% |
| Ti64 | 795 | 115 | | | 1034 | 150 | 10% |
| 904L | 220 | 31 | 250 | 36 | 490 | 71 | 35% |

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